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Perspectives on geologic carbon storage

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Geologic carbon storage (GCS) is a fundamental pillar of carbon management that helps mitigate greenhouse gas emissions and addresses the negative effects of climate change. Viable CO₂ storage sites share some of the same elements required for successful petroleum systems. For example, while reservoir, seal, and trap are required, migration pathway and timing are not important for CO₂ storage, because rather than withdrawing fluid from a trap, CO₂ storage involves injection into a geologic trap. Conceptually, this represents a form of reverse production. Numerous petroleum traps around the world, as well as naturally occurring CO₂-producing fields and natural gas storage sites attest that safe, long-term storage is possible. Research over the past two decades identified five methods of Geologic Carbon Storage which have been validated through several demonstration and pilot projects around the world: (1) storage in depleted oil and gas fields, (2) use of CO₂ in enhanced hydrocarbons recovery (3) storage in saline formations/aquifers, (4) injection into deep unmineable coal seams, and (5) *in-situ/ex-situ* carbon mineralization. The greatest volumetric potential for GCS is found in saline aquifers which are present throughout the world's sedimentary basins.

KEYWORDS

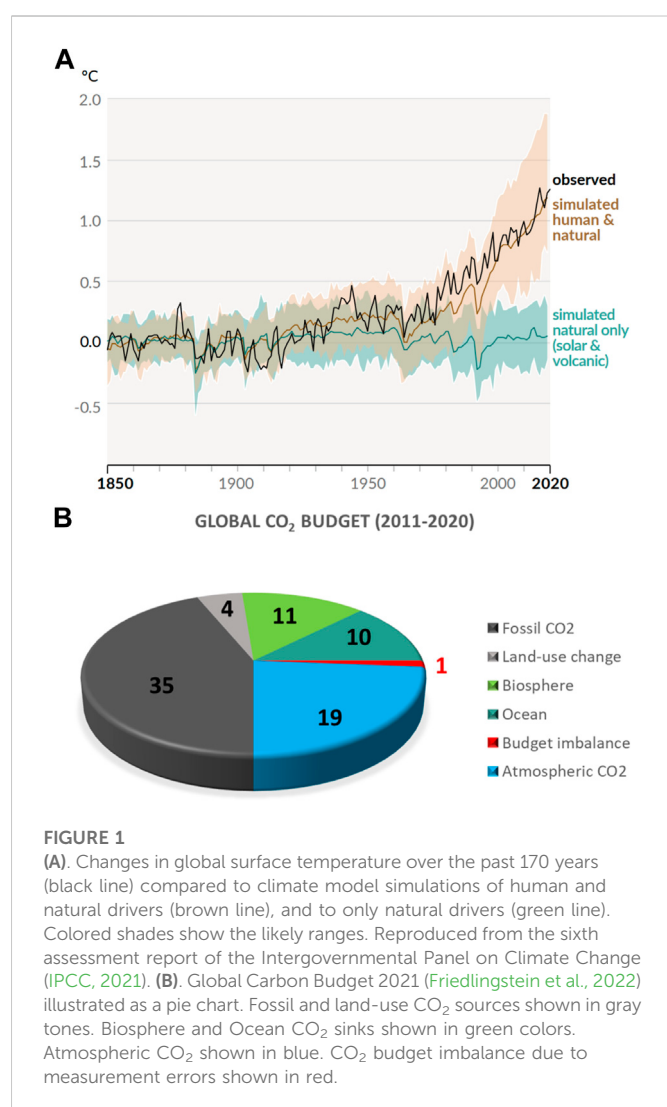
geologic carbon storage (GCS), carbon management, subsurface, geology, aquifers

1 Introduction

It is now widely believed that human CO₂ emissions have thrown the natural carbon cycle, where CO₂ resulting from all natural and anthropogenic carbon sources is taken up by CO₂ sinks, out of balance. As a consequence, a large fraction of the approximately 39 Gt of CO₂ that are emitted on an annual basis resides in the atmosphere (Friedlingstein et al., 2022). A recent report published by the Intergovernmental Panel on Climate Change (IPCC) concluded unequivocally that human influence resulted in unprecedented climate warming, and that the warming is driven by greenhouse gas emissions (IPCC, 2021). Figure 1A illustrates the observed and modeled warming since 1850 and clearly demonstrates the temperature response to human and natural factors. Figure 1B shows the perturbation of the global carbon cycle caused by anthropogenic activities resulting in the addition of about 19 GtCO₂ to the atmosphere per year (Friedlingstein et al., 2022).

This article provides a current snapshot of geologic carbon storage (GCS) options. What is carbon dioxide (CO₂)? As is commonly known, CO₂ is a colorless, odorless, and incombustible gas at atmospheric pressures and room temperature. CO₂ results from the oxidation of carbon and is produced during respiration by all animals, fungi, and microorganisms. It is used in a variety of industries, for example as a solvent (Valluri et al., 2022), an anesthetic, a food packaging gas (Lee et al., 2016), and a refrigerant (Bansal et al., 2012). Most relevant to this study, CO₂ forms by burning of fossil fuels and it enters the atmosphere as an important greenhouse gas.

First, we summarize the defining characteristics of a successful geological CO₂ storage site. Subsequently, five proven methods of geological CO₂ storage are briefly discussed: (1) Depleted



oil and gas reservoirs, (2) Use of CO₂ in enhanced hydrocarbon recovery, (3) Saline formations/aquifers, (4) Coal seams, and (5) *In-situ/ex-situ* carbon mineralization.

2 Characteristics of a successful CO₂ storage site

Before examining the geological CO₂ storage site requirements, the elements of a successful petroleum system are presented in a simplified manner. The genesis of a petroleum system begins with the deposition of a source rock rich in organic matter. Afterwards, a reservoir rock with the potential to preserve appropriate porosity and permeability upon burial is deposited. The sedimentation sequence ends with a seal unit, commonly referred to as cap rock, with very low porosity and permeability. Figure 2A captures this sedimentary sequence. The next step in the development is an event that creates a petroleum trap. For example, folding associated with horizontal compression can create anticline shapes, which often act as traps. Sometimes, however, seals are deposited after trap formation or even after partial erosion have taken place. Successive deposition of sediment layers leads to progressively deeper burial of the source

rock. Due to the geothermal gradient, at a certain burial depth, temperatures are sufficiently high to convert kerogen in the source rock to hydrocarbons. In order to fill the trap with oil and/or gas, a migration pathway has to be present. Figure 2B illustrates these elements. Lastly, the relative timing of all of the above steps needs to be favorable for a successful petroleum system to form. For example, if burial is not deep enough for maturation to occur, or if a seal rock is deposited after migration, a trap will not be filled because petroleum would not have formed or it would have escaped, respectively.

A successful CO₂ storage site necessitates the same elements as a petroleum system, except a source rock and a migration pathway. In other words, a CO₂ storage site requires a reservoir rock, a seal rock, and a trapping configuration.

Another key difference with hydrocarbon projects is the requirement to characterize and monitor seal performance because seal efficacy is unknown unless it has been geologically proven by the presence of hydrocarbons or some other trapped fluids, for example *via* pore pressure measurements. In addition to data acquisition at the site characterization stage, long-term monitoring should be put in place to prove that any CO₂ leakage from the sequestration site is zero or within allowable tolerance (Roberts and Stalker, 2020).

Clearly, the existence of petroleum traps around the world demonstrates that buoyant fluids such as oil or gas can be entrapped for millions of years in the subsurface. Besides entrapping petroleum fluids, geologic structures can also trap CO₂. As a result of magma degassing and metamorphism of carbonates, naturally occurring CO₂ fields are present on nearly all continents (Holloway et al., 2005; Miocic et al., 2016). Some of these fields have stored CO₂ for up to 70 million years (Stevens and Tye, 2007), proving that CO₂ storage in geologic formations is not only technically viable but it is in fact a natural process. Several natural CO₂ fields are commercially exploited, for instance, to enable CO₂-enhanced oil recovery (EOR) in petroleum fields. For example, the McElmo Dome in Colorado, United States, contains approximately 1.6 billion tons of nearly pure CO₂ (96%–98%) and produces about 15 million tons per year from 41 wells (Zabel, 1955; Thomaidis, 1978; Gerling, 1983; Cappa and Rice, 1995; Stevens et al., 2005). CO₂ from McElmo Dome has been re-injected for EOR in the Permian Basin, Texas, for more than 30 years (Holloway et al., 2005; Stevens et al., 2005). McElmo Dome is generally viewed as the best analog for geologic CO₂ storage sites for depleted oil and gas fields (Stevens et al., 2005; Stevens and Tye, 2007).

CO₂ at McElmo Dome is stored in a 75–90 m thick lower Carboniferous carbonate reservoir at about 2,300 m depth. The overlying caprock consists of 400 m thick halite and there is no evidence of CO₂ leakage into overlying strata (Stevens et al., 2005). Several faults perturb the reservoir, but they do not extend across the caprock. Figure 3 illustrates the geological key aspects of McElmo Dome. Although McElmo Dome may be the most commonly cited example of a natural CO₂ field, there are several others that are well documented, such as the St. Johns field, Arizona/New Mexico (Holloway et al., 2005), and the Bravo Dome in New Mexico (Sathaye et al., 2014).

Furthermore, natural gas has been stored in depleted oil and gas reservoirs (e.g., Stuart, 1991), saline formations, and salt caverns for almost 100 years and in many parts of the world to provide for peak demand and to balance seasonal fluctuations in gas supply (IPCC, 2005). The great majority of storage projects are safe and successful, though a few have leaked gas, due to well integrity issues or leaky faults

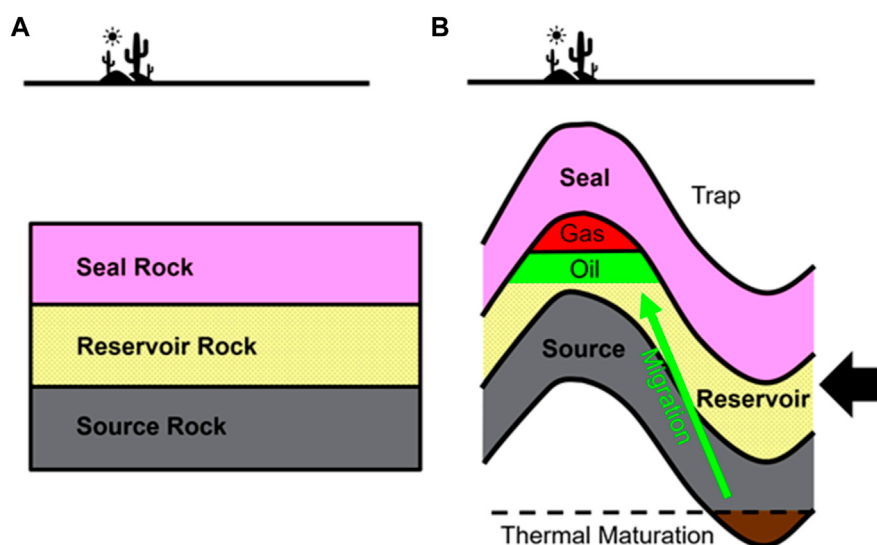


FIGURE 2

Simplified illustration of the key elements of a successful petroleum system. (A). Deposition of source, reservoir, and seal rocks. (B). Folding creates a petroleum trap. A migration pathway must exist to fill a trap with oil and/or gas.

(IPCC, 2005). Gas storage projects are typically more complex than CO₂ storage projects because of the highly flammable and explosive properties of gas, and there are highly variable but sometimes frequent cycles of injection and extraction. CO₂ leakage risk is high if concentrations are high (Holloway et al., 2007), or if pressures are high, for instance in pipeline and injection systems (Huang et al., 2014). Also, a number of these facilities, such as the Berlin Natural Gas Storage Facility (IPCC, 2005), are in areas of high population density, which would not be the case for a remote onshore or an offshore CO₂ sequestration site. Therefore, in addition to natural CO₂ fields, existing natural gas storage facilities in geologic formations offer excellent opportunities to study and design CO₂ sequestration sites. In addition, much can be learned about seal capacity and storage potential from ongoing research devoted to hydrogen storage in salt caverns and porous formations (e.g., Matos et al., 2019; Lankof et al., 2022). In the following section, five methods of geologic carbon storage are discussed briefly.

3 Geologic carbon storage options

Five methods of geologic carbon storage have been shown to be technically viable, and some are employed as pilot, demonstration, or even full-scale projects (the majority of active projects in the 25 years to date are reviewed by Zhang et al., 2022): (1) storage in depleted oil and gas fields, (2) use of CO₂ in enhanced hydrocarbon recovery, (3) storage in saline formations/aquifers, (4) injection into deep unmineable coal seams, and (5) *in-situ/ex-situ* carbon mineralization. Each of these methods is briefly described below.

3.1 Carbon storage in depleted oil and gas fields

Depleted oil and gas reservoirs are commonly viewed to be excellent sites for CO₂ storage for several reasons (Jenkins et al.,

2012): (1) They prove long-term hydrocarbon retention by demonstrating the capacity for buoyant fluids to be trapped in the subsurface, (2) the structure and properties of oil and gas fields have been extensively studied, (3) there usually is widespread documented production history, and (4) the existing infrastructure and wells may be used for handling CO₂ operations (IPCC, 2005). Despite geomechanical effects owing to reservoir compaction, carbon storage in depleted fields can be thought of as “reverse production”. Despite the technical appeal, however, no large-scale CO₂ storage projects in depleted reservoirs have been deployed anywhere in the world. A few CO₂ injection pilot projects have been completed, with monitoring still ongoing, such as the Otway project in Australia (Underschlutz et al., 2011). However, their total stored CO₂ volume is relatively small compared to the required storage volumes of industrial-scale sequestration projects. A further problem with repurposing ageing or abandoned hydrocarbon fields is that the wellbore integrity is unknown. Large hydrocarbon fields may have thousands of drilled wells and the quality of annular cement may have deteriorated since the well was drilled or may never have been documented in the first place (Zhang and Bachu, 2011). As a result, the top seal that originally trapped hydrocarbons and is a key feature of the longevity of CO₂ sequestration may have been compromised by many hundreds of human-made channels (Davies et al., 2014; Kiran et al., 2017).

For example, the Lacq-Rousse project in southwestern France aims to demonstrate the technical feasibility and reliability of an integrated CO₂ capture, transportation, injection and storage effort (Prinet et al., 2013). From 2009 to 2013, 51,000 tons of CO₂ were injected into a carbonate reservoir at 4500 m depth. The reservoir is overlain by a mudstone formation. A comprehensive monitoring plan was implemented, some stages of which are still ongoing. Monitoring encompasses CO₂ stream composition, CO₂ atmospheric concentration at the injection well, well annulus pressure, pressure and temperature along the injection well and in the reservoir, microseismicity, soil gas, ground and surface water quality, and fauna and flora biodiversity. To date, no CO₂ leakage has been identified.

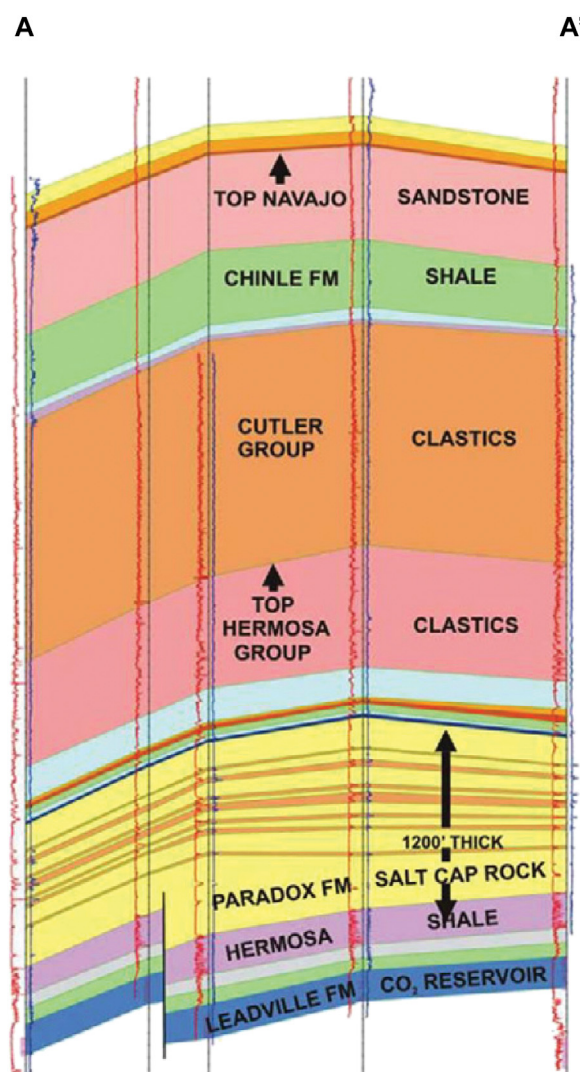


FIGURE 3

Simplified cross-section of the McElmo Dome (Stevens, 2005), illustrating the geometric arrangement of the carbonate reservoir (Leadville Limestone) containing CO₂, the overlying evaporite caprock (Paradox Formation), and one fault affecting the reservoir but not the seal.

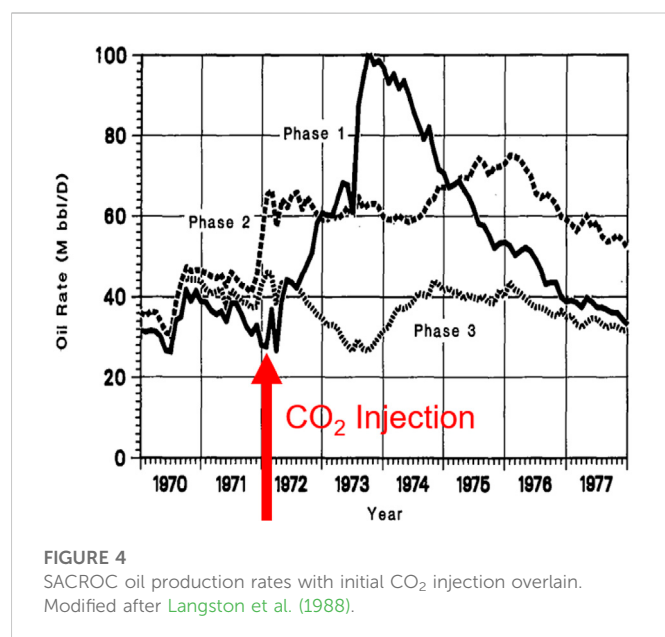
Another example of a completed small-scale CO₂ demonstration storage project in a depleted reservoir is the Otway project in Australia. From 2008 to 2011, 65,000 tons of CO₂ were injected into a depleted sandstone reservoir that is capped by a mudstone (Cook, 2014). Similar to Lacq-Rousse, an extensive monitoring program was deployed. Seismic monitoring was conducted, but due to the low volume of CO₂ injected, it was not detected. Microseismic as well as pressure and temperature sensors in the monitoring well failed, limiting the data collection to the injection well (IEAGHG, 2017). Successful groundwater monitoring, logging, and analyzing downhole fluid samples showed containment of CO₂ in the subsurface.

3.2 Use of CO₂ in enhanced hydrocarbon recovery

CO₂ enhanced oil recovery (EOR) is a technology applied to depleting oil reservoirs in order to enable additional oil recovery and extend the field

life. The main principles of CO₂-EOR rely on the fact that CO₂ acts as a solvent and that it is miscible with oil, while water and oil are immiscible. CO₂ causes oil to swell and lower its viscosity, allowing more oil to flow to a producing well (NETL, 2010). It is important to understand that the boundary between depleting and depleted reservoir is often unclear. For instance, the technical and economic limits to recovery may vary significantly based on the geography, the local regulatory framework, production methods and history, and the geologic attributes of the formation. In contrast to the additional cost without return associated with carbon storage in depleted fields, CO₂-EOR in depleting fields usually is desirable because it increases profitability.

CO₂-EOR was first used in 1972 in the SACROC (Scurry Area Canyon Reef Operators Committee) Unit in the Permian Basin in Texas (Langston et al., 1988). Due to very low recovery efficiency (~4.5% of the original oil in place), as a result of rapidly dropping reservoir pressure, CO₂-EOR was identified as a means to improve recovery. Shortly after CO₂ injection was initiated in 1972, oil production rates improved substantially (Figure 4). As of 2019,



about 150 Mt of CO₂ were injected into a Permian carbonate reservoir. 75 Mt of CO₂ were recovered and recycled, with the balance to be permanently sequestered. Field-based groundwater studies by the Gulf Coast Carbon Center concluded that, despite > 35 years of CO₂ injection, drinking water quality has not been adversely impacted (Gerling, 1983).

Another successful CO₂-EOR project was conducted in the Weyburn Field in Canada. Weyburn is a large international research project supported by 15 industry and government

sponsors and consulting organizations with a budget of about 40 million Canadian Dollars (Preston et al., 2005). More than 35 million tons of CO₂ have been injected since 2000, with a target of 45 million tons (Sacuta et al., 2015). It is estimated that an additional 130 Mbbls of oil will be recovered via CO₂-EOR, extending the field life by 25 years. Figure 5 schematically illustrates the geological configuration of the Weyburn field.

A further example of a CO₂-EOR demonstration project is the Uthmaniyah Field, Saudi Arabia (Kokal et al., 2016). More complex CO₂ injection scenarios involving water-alternating-gas injection for EOR have been considered, but demonstrations are not yet available (Wang et al., 2020).

How much CO₂ is permanently sequestered during CO₂-EOR and does this amount offset the CO₂ emitted during the operation? It is important to recognize that CO₂ emissions result from energy consumption throughout an EOR operation as well as from the transport, processing, and combustion of the additional oil produced. During CO₂-EOR the produced CO₂ is separated, re-injected into the reservoir, and the process is repeated in a loop. Hence, quantifying the ultimate CO₂ storage capacity of EOR projects begs the question of whether the oil can be classified as Net Carbon Negative (Nuñez-López et al., 2019). A recent study examined multiple CO₂-EOR scenarios and found that all of them start operating with a negative carbon footprint but ultimately generate a positive carbon footprint (Nuñez-López et al., 2019). The authors also found that the net carbon balance is highly variable among different EOR settings and also through time within a single setting. For these reasons, it is desirable to conduct an analysis of expected CO₂ footprint (for any carbon storage method) from start to closure of an operation and seek opportunities to continuously optimize CO₂-EOR and geologic carbon storage.

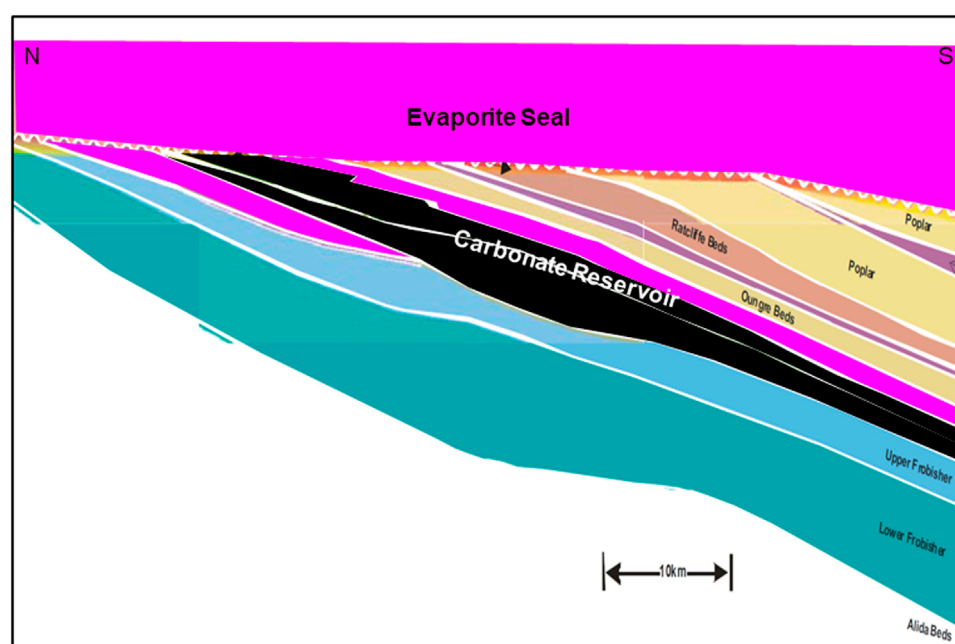


FIGURE 5
Simplified representation of the geological configuration of the Weyburn CO₂-EOR site in Canada. Carbonate reservoirs are shaded black. Evaporite seal units are shown in magenta. Inset shows how CO₂ flooding is forecasted to recover additional oil volumes extend the field life (Modified after Whittaker, 2005; Erikson, 2020).

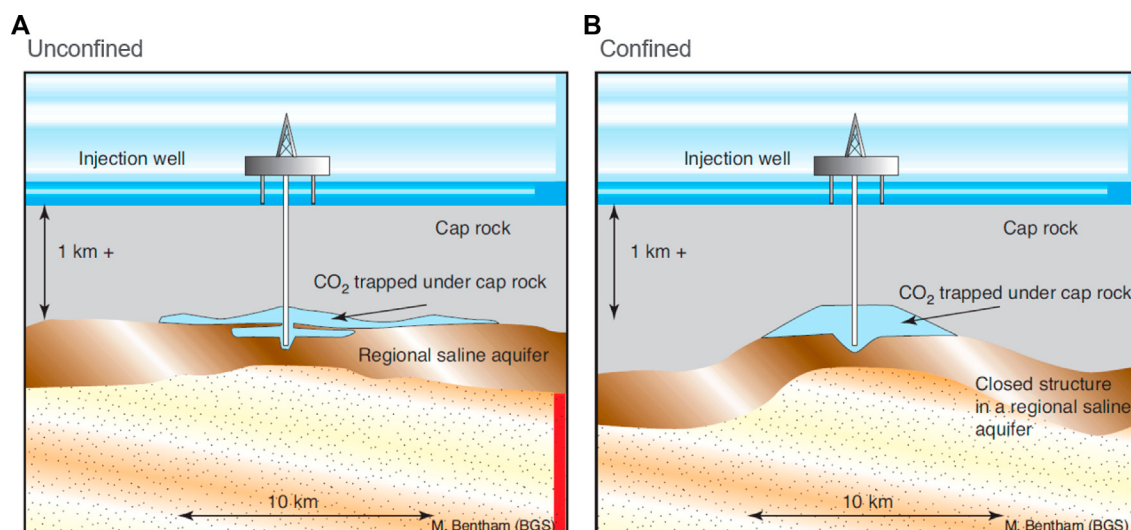


FIGURE 6
Conceptual representation of geologic CO₂ storage in open (A) and closed (B) saline aquifers (Bentham and Kirby, 2005).

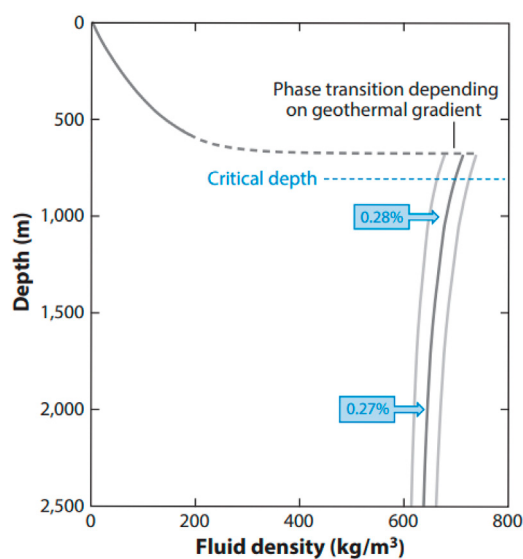


FIGURE 7
CO₂ density versus depth for a geothermal gradient of 35°C/km ($\pm$ 2°C/km; gray lines) and hydrostatic pore pressure. CO₂ transitions from gas to a supercritical fluid between 550 m and 750 depths, depending on temperature. Blue boxes show the relative volume of CO₂ at depth compared to surface volumes (Ringrose et al., 2021).

Analogous procedures for enhanced gas recovery (EGR) is less widely practiced but some demonstration projects exist (Liu et al., 2022). In this scenario, CO₂ is injected close to the base of the gas column and provides additional pressure and piston displacement of the gas towards updip producers. Three demonstration projects exist to date, the longest running being the K12-B project in the Dutch North Sea which began injecting CO₂ in 2004 and has

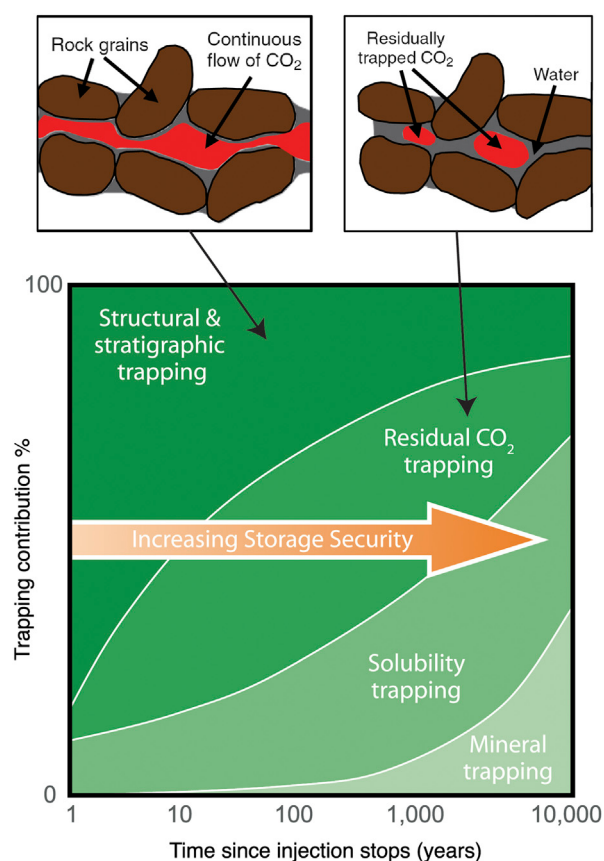


FIGURE 8
Conceptual representation of how the contribution of CO₂ trapping mechanisms change with time when CO₂ is injected as a supercritical fluid (Modified after IPCC, 2005; Garcia et al., 2010; Snæbjörnsdóttir et al., 2020).

injection potential of approximately 20 kt per year (Vandeweyer et al., 2020).

3.3 Geologic carbon storage in saline formations/aquifers

Saline formations or aquifers are any sedimentary layers with brines containing high concentrations of dissolved salts, making them unsuitable for use as drinking water. Typically, the amount of total dissolved solids in such formations exceeds 10,000 mg/L (Garcia et al., 2010). Carbon storage in saline aquifers generally requires the same geological elements as depleted oil and gas fields and/or depleting reservoirs, namely, a CO₂ storage reservoir with sufficient porosity and permeability, a sealing cap rock, and a trapping configuration. However, very broad and gently folded, or even flat geometries are suitable as well. These saline aquifers may be confined (valid topseal) or unconfined (no topseal, fluid fill extends up to the water table) (Bentham and Kirby, 2005; Woessner And Poeter, 2020). The terms “open” and “closed” are sometimes used in relation to saline aquifers. These terms may refer to structural closure or whether or not the aquifer is laterally confined (open if not, closed if so). Figure 6 illustrates open and closed structural configurations schematically.

Due to their ubiquitous occurrence in sedimentary basins on all continents, saline formations/aquifers have the greatest potential for large-scale carbon storage (Bentham and Kirby, 2005; Michael et al., 2010; Shukla Potdar and Vishal, 2016; Ringrose et al., 2021). The reservoir must be at least approximately 800 m deep so that the pressure at these depths causes a phase transition of CO₂ from gas to a supercritical fluid with much higher density, illustrated in Figure 7 (Ringrose et al., 2021). Storing dense CO₂ in this manner decreases its volume many times (CO₂CRC, 2021), thus dramatically increasing the storage capacity of a saline aquifer (and any other potential storage reservoir with pore space).

Several trapping mechanisms occur in saline formations some of which are common to other settings, such as depleted hydrocarbon reservoirs: (1) Structural and stratigraphic trapping, where CO₂ exists as a continuous fluid and it can flow, (2) residual trapping, as non-connected, isolated CO₂ pockets, (3) solubility trapping, which is synonymous with dissolution trapping, and (4) mineral trapping, which involves chemical reactions and the formation of carbonate minerals (Snæbjörnsdóttir et al., 2020). With time, CO₂ can progress from structural/stratigraphic trapping all the way to mineral trapping thus progressively increasing the storage security. The time dependency of these four known trapping mechanisms is conceptually demonstrated in Figure 8. Timing and CO₂ volumes associated with these mechanisms are uncertain.

The world's first large-scale, industrial capture and offshore effort to store CO₂ in a saline formation is the Sleipner project in the North Sea. Since 1996, Norwegian operator Equinor (FKA Statoil) has been injecting CO₂ into the ~200 m thick Utsira Sands at depths of 900–1000 m (Arts et al., 2004). The source of the CO₂ is production of a condensate gas in the deeper Heimdal Formation (~2500 m) with approximately 9% CO₂ content. Due to a carbon tax in Norway, the operator and partners decided to sequester the CO₂. An extensive geophysical and environmental monitoring program has been deployed. At the time, there were no monitoring guidelines or requirements imposed (storage and monitoring regulations in Norway became active in 2014), and so the operating companies opted for a

large variety of methods with regular repeats and dense coverage. No CO₂ leakage has been detected.

4D seismic (AKA time-lapse 3D seismic) and gravity monitoring were conducted to track the CO₂ plume *via* velocity and density changes compared to the initially brine-filled reservoir (Furre et al., 2017). 3D seismic surveys were conducted in 1999, 2001, 2002, 2004, 2006, 2008, 2010, 2013, and 2016, and this provided an excellent dataset to seismically image the position and shape of the CO₂ plume (See Figure 1 in Oudinot et al., 2017) (See Figure 2 in Furre et al., 2017).

High-precision gravity monitoring was conducted as well to provide an independent measurement of density changes. This effort confirmed the time-lapse seismic determined plume outline, and, within measurement uncertainty, that the amount of detected supercritical CO₂ equals the injected amount (Furre et al., 2017).

CO₂ injection scenarios or concepts often involve siliclastic reservoirs but many world-class reservoirs and aquifers are carbonates so CO₂ interaction with limestone reservoir represents an uncertainty and opportunity to unlock additional potential in saline aquifer sequestration (Raza et al., 2020).

3.4 Geologic carbon storage in coal seams

Coal seams are dual porosity systems characterized by (1) matrix porosity, and (2) fracture (cleat) porosity (IPCC, 2005; Liu et al., 2018). This co-existence of matrix micropores and open fractures provides for very efficient storage mechanisms for adsorbing a variety of gases, including methane and CO₂ (IPCC, 2005). Methane moves within and through coal by diffusion in the matrix and Darcy flow in the fractures (Kou et al., 2021). Storage options for CO₂ in coal beds comprise injection into what is generally characterized as deep, unmineable coal seams and CO₂-Enhanced Coal Bed Methane (ECBM).

Coal beds are classified as unmineable if they meet the following criteria: too thin, too deep, too unsafe for mining operations, too high in sulphur or mineral matter, too low in grade (Bachu, 2007). It is important to understand that the criteria used to determine a viable depth range for unmineable coal beds that are, however, suitable for CO₂ storage are not consistently defined. For instance, candidate coal beds should be deeper than any groundwater aquifers and deeper than any coal beds that are mined in the future. A depth window is defined locally in central and southern Alberta between a ceiling, based on water well depths, of 300 m and, based on the CO₂ phase transition from gas to supercritical fluid, a floor of 800–900 m (Bachu, 2007). Similar to CO₂-EOR applied in oil fields, geological carbon storage in coal seams is often seen as a win-win technology, because two benefits are simultaneously realized: (1) increase the production of coal bed methane, and (2) leave CO₂ behind in the pore space for permanent sequestration. CO₂-ECBM works by gas exchange in the coal matrix. When methane is produced by thermal maturation, it adsorbs onto surfaces in the coal matrix. CO₂ has greater adsorption capacity in coal compared to methane. Therefore, if CO₂ is injected into coal, it causes desorption of methane, which is released into the cleats and subsequently replaced in the matrix by CO₂.

Proof-of-concept of CO₂-ECBM was achieved in 1972 through laboratory work which demonstrated removal of methane from crushed coal by streaming CO₂ through it (Every and Dell'osso Jr., 1972). However, a recurring issue with injecting CO₂ into coal beds is swelling of the matrix, reducing the cleat aperture, thereby

significantly reducing the permeability for methane flow in the cleat network (Oudinot et al., 2017). N₂ has lower adsorption capacity than methane. As a result, N₂ has the opposite effect on coal matrix volume: the coal matrix shrinks, cleat aperture is opened, and permeability increased. Hence, one way to improve the efficiency of CO₂-ECBM is to explore the amount, timing, and frequency of N₂ injection before CO₂ injection, or in an alternating fashion.

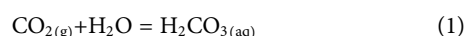
Priming coal with certain chemicals can potentially result in much greater CO₂ storage. For instance, the substance methyl orange can increase the CO₂ adsorption potential of coal nearly ten times (Abid et al., 2021). Methyl orange is a classic dye used in a number of industries, such as textile, paper, rubber, cosmetic, wool, and nylon. This substance is often released into the hydrosphere as a pollutant. Making use of it as an adsorption catalyzer for CO₂ in coal could realize two benefits, namely sequestering CO₂ in coal as well as safely disposing methyl orange (Abid et al., 2021).

3.5 *In-situ* and *ex-situ* carbon mineralization

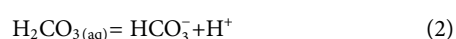
Conceived as novel concepts in the 1990s, mineral trapping of CO₂ (Figure 8) via artificially induced carbon mineralization is an accelerated form of naturally occurring chemical fixation of CO₂ in the form of solid carbonate minerals (Seifritz, 1990; Lackner et al., 1995; Kelemen et al., 2019). During this process, chemical reactions form calcium, magnesium, and iron carbonates. The resulting minerals are identical to the naturally occurring equivalents, which have been stable for millions of years (Lackner et al., 1995).

The geochemistry of mineral carbonation is well understood and comprises the following general steps (Aradóttir et al., 2011):

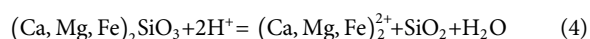
Step 1: Dissolution of CO₂ in water forms carbonic acid.



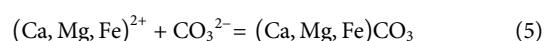
Step 2: Carbonic acid dissociates into bicarbonate and carbonate according to:



Step 3: Dissolution of cations takes place when Ca-, Mg-, and Fe-bearing silicate minerals come in contact with this acidic fluid.



Step 4: The free cations Ca, Mg, and Fe react with carbonate and precipitate carbonate minerals according to:



Ca-, Mg-, and Fe-bearing silicate minerals, such as plagioclase, pyroxene, and olivine, are found in mafic and ultramafic rocks, such as basalt and peridotite, and they are present in large quantities in pulverized form in mine tailings and other industrial waste products. Currently, *in-situ* and *ex-situ* mineral carbonation operations employ injection of CO₂ (dissolved in water or as liquid or supercritical fluid) into basalt, and exposing ground reactive rock to CO₂ in a gas stream, respectively (Snæbjörnsdóttir et al., 2020).

Creating new carbonate minerals using these techniques essentially mimics natural weathering, albeit at a faster rate under ideal circumstances when reactions rates can be accelerated (Kelemen et al., 2019; McQueen et al., 2020).

3.5.1 *In-situ* carbon mineralization

In-situ carbon mineralization takes place in the subsurface by injection of CO₂ into compositionally and structurally suitable rocks. As described in the previous section, CO₂ reacts with formation water and any divalent cations that are present to form stable carbonate minerals.

Two field studies were undertaken to demonstrate the feasibility of *in-situ* carbon mineralization in basalt: The CarbFix project in Iceland (a combined industrial-academic pilot project), which is still active, and the smaller-scale Wallula pilot project in Washington, United States, during which 1,000 tons of CO₂ were injected in 2013 (Snæbjörnsdóttir et al., 2020). The CarbFix method utilizes the dissolution of CO₂ in water during injection, whereas the Wallula project exercises injection of pressurized, liquid CO₂ (Snæbjörnsdóttir et al., 2020). The CarbFix project demonstrated that *in-situ* carbon mineralization is technically feasible and also practical at operational timescales. For example, more than 95% of the injected CO₂ was mineralized in less than 2 years (Matter et al., 2016). The CO₂ utilized in the CarbFix project is a byproduct of geothermal water production at the Hellisheiði geothermal power plant (Gunnarsson et al., 2018). The Carbfix project maintains a website showing the daily as well as the total cumulative volumes of CO₂ injected (Carbfix, 2021). As of 10/6/2021, roughly 72,500 tons of CO₂ have been injected since 2014. In contrast, the Wallula pilot was a much smaller demonstration project. Over a 2 months period in 2013, approximately 1,000 tons of CO₂ were injected into brecciated basalt capped by basalt (White et al., 2020). A blend of hydrological tests and numerical modeling indicated that about 60% of the injected CO₂ was mineralized within 2 years (White et al., 2020).

In-situ carbon mineralization has the potential for widespread upscaling, for example in regions with buried basaltic volcanoes and lava fields (Holford et al., 2021). However, temperatures exceeding 250°C in geothermal fields may potentially induce decarbonation reactions at depths greater than 1300 m (Clark et al., 2020). Effective monitoring techniques and water requirements are also uncertain (Raza et al., 2022).

Figure 8 illustrates that *in-situ* carbon mineralization (mineral trapping) likely occurs associated with other carbon storage methods as well, such as in saline aquifers, as long as the rock composition allows for the above quoted chemical reactions to occur. Note however, that meaningful contributions from this process do not occur until hundreds to thousands of years have passed since initial injection as a supercritical fluid. Hence, it is difficult, if not impossible, to quantify and control the exact contributions of *in-situ* mineralization as one contributor amongst others in a carbon storage project. On the other hand, the CarbFix and Wallula projects mentioned above demonstrate that targeted CO₂ injection in basalt achieve predictable mineralization on short timescales, on the order of years, thus making such projects very viable from planning and operational perspectives.

3.5.2 *Ex-situ* carbon mineralization

By contrast to subsurface operation of *in-situ* carbon mineralization, *ex-situ* carbonation mineralization is run above ground. This method involves the reaction of a suitable feedstock

(such as fly ash, waste from the steel and iron industries, ground reactive rock, and mine tailings) with CO₂ in a gas stream (Snæbjörnsdóttir et al., 2020). The resulting stable carbonate minerals are disposed subsequently. Owing to the much higher cost of *ex-situ* compared to *in-situ* carbon mineralization associated with grinding and transporting the feedstock (Kelemen et al., 2019; Snæbjörnsdóttir et al., 2020), this technology is not widely used currently. Nonetheless, due to the high technical viability, there likely is large potential for this technology to be employed in the future (Picot et al., 2011). In addition, technologies beyond CO₂ gas floods are being developed (Yadav and Mehra, 2021), and there is even potential for repeat direct air capture of CO₂ using *ex-situ* mineralization of magnesite (McQueen et al., 2020). *Ex-situ* carbon mineralization may be particularly applicable in the mining industry, where large volumes of rocks are crushed and pulverized. For example, kimberlite mines yield enormous amounts of fine-grained tailings from processing ultramafic rocks that are composed of silicate minerals, such as serpentine, olivine, brucite, and smectite. Recent work shows that *ex-situ* carbonation of 4.7–24.0 wt% of annually processed kimberlite could offset 100% of carbon dioxide equivalent emissions of the mines investigated (Mervine et al., 2018).

One potential disadvantage of permanently locking up CO₂ in carbonate minerals is that it cannot be retrieved from the sequestration site, should there be a profitable market for CO₂ as a commodity in the future. The energy required for reversing the mineralization process and releasing CO₂ again is substantial (Lackner et al., 1995) and would likely defeat the purpose of removing it from the atmosphere.

4 Analysis of geologic carbon storage sites

The principal purpose of structural geological and geomechanical characterization of potential CO₂ storage sites is to ensure hydraulic integrity of the geological formations into which CO₂ is injected and the ones around it (Hawkes et al., 2005). This can be achieved by describing the structural geometry, for example through identifying potential leak points, spill points, as well as potential pathways along which CO₂ may escape to undesired formations and/or the atmosphere, and establishing the hydrodynamic conditions in the reservoir (Larkin, 2010). In addition, CO₂ injection increases the pore pressure in the reservoir, which alters the state of stress in the near and far fields, which can trigger fault reactivation, create new fractures, and thus induce seismicity (Burghardt, 2017).

A useful way to help illustrate the concept of structural geometry for laypersons is to conduct a thought experiment with a hypothetical marble run (Figure 9). Imagine placing a marble on the top ramp and trying to predict which path the marble will take until it ultimately ends up on the bottom ramp (Figure 9A). A special condition in this marble run is a thin paper membrane on the third ramp (from top) that cannot hold the weight of the marble. The marble will break the membrane and drop down to the next lower ramp. This represents a transmissibility barrier. Now turn the marble run upside down (Figure 9B). Repeat the thought experiment and imagine that the marble is buoyant so that it will move upwards. The upside-down marble run is an excellent analog for petroleum and CO₂ trap analysis.

Now imagine that the marble represents a buoyant hydrocarbon or CO₂ fluid molecule. Forecasting the upward path of the marble is akin to predicting the migration pathway of a fluid in the subsurface. The migration pathway can be along permeable sandstone or limestone units that are separated by impermeable shale or evaporite seal units (analogous to the black ramps in this experiment). Faults may juxtapose either sandstone/limestone on seal creating a sealing configuration, or sandstone/limestone on itself or another sandstone/limestone unit, creating a leaking configuration. The paper membrane in Figure 9B may represent a leak point in the subsurface shaped by fault juxtaposition. Upward flow will continue until an ultimate geometric trapping configuration is encountered.

A number of potential leak points can exist in geological CO₂ storage sites (Figure 10). For example, faults can juxtapose reservoir on reservoir or act as fluid conduits themselves, hydraulic fractures can affect and compromise the seal above a storage reservoir, and there may be cement issues in a well connecting two adjacent or stacked reservoirs (Hawkes et al., 2005). These and similar issues can cause inadvertent CO₂ migration from an intended storage reservoir to an unintended porous formation, such as an aquifer, and ultimately to the surface and into the atmosphere.

When CO₂ and formation water coexist as separate phases during structural, stratigraphic, or residual trapping in a geologic formation (Figure 8), capillary processes determine the column height of the CO₂ body (Ringrose, 2020). The physics of capillary trapping is well understood and the height of a gas column that can be held against gravity by the capillary entry pressure of the seal rock can be calculated according to (Berg, 1975):

$$z_g = \frac{2\gamma \cos \theta \left(\frac{1}{r_{cap}} - \frac{1}{r_{res}} \right)}{g(\rho_w - \rho_g)} \quad (6)$$

where r_{cap} and r_{res} are the pore throat radii in the cap rock and reservoir, respectively, γ is the interfacial tension, θ is the fluid contact angle, and ρ_w and ρ_g are the water and gas densities, respectively. CO₂ column height is one important input for determining the CO₂ storage volume of a potential site. As can be seen from Eq. 6, a large difference between the pore throat radii of the cap rock and reservoir and a small density contrast between water and gas yield a large gas column, whereas a small difference in pore throat radii and a large density contrast achieve a small column.

The risk for fault reactivation can be assessed using simple Mohr-Coulomb theory. The slip tendency T_s of an existing fault in the subsurface can be calculated if the shear and normal stresses on the fault plane, τ and σ_n , as well as the pore pressure, P_f , are known, according to (Streit and Hillis, 2004):

$$T_s = \frac{\tau}{\sigma_n - P_f} \quad (7)$$

Eqs. 6, 7 are useful for determining CO₂ column height and fault slip tendency for screening purposes and to help identify and rank the most viable and lowest risk candidates among a portfolio of potential storage sites.

It is important to understand that the *in-situ* stress state exerts a first-order control on the geomechanical behavior of rocks during CO₂ injection. While the approaches summarized above provide first-order answers, they are limited to one-dimensional analysis and assume

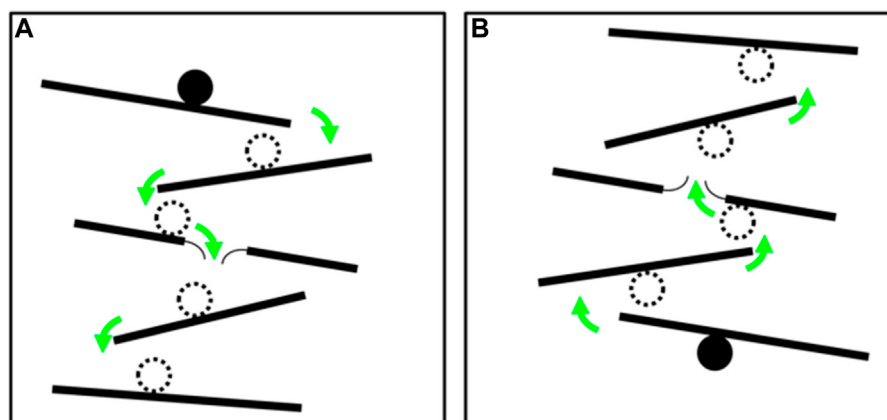


FIGURE 9

Schematic illustration of a hypothetical marble run. Green arrows show the path the marble will take when placed on the top ramp. (A). Right-side up. A thin paper membrane on the third ramp represents a potential leak point if the marble weighs more than the membrane can hold. (B). Upside-down marble run representing the concept of trap analysis for a buoyant fluid, such as petroleum or CO₂.

spatially homogeneous as well as uniform rock properties and behaviors. Quasi-one-dimensional simplifications, as often used in the petroleum industry, are inaccurate (Burghardt, 2017). Stress is a three-dimensional tensor, and thus characterizing a potential CO₂ storage site more comprehensively and accurately requires three-dimensional geomechanical modeling. Three-dimensional geomechanical modeling provides the ability to incorporate fault plane orientation, *in-situ* stress orientations and magnitudes, pore pressure, spatial variation in reservoir and seal parameters, and wellbores in the investigation. Seamless integration of geomechanical modeling with reservoir modeling and simulation is highly desirable to capture the production history as well as the spatial distribution of porosity and permeability.

Inventorying, screening, and selecting a site in the first place is a portfolio development and optimization process akin to any other kind of resource exploration. However, carbon sequestration is not a

mature line of subsurface engineering and there are few documented cases where a full cycle of exploration through delineation and project execution has been achieved. There have been a number of portfolio development cases (Bentham et al., 2014; Gruson et al., 2015). Although free from the constraints of hydrocarbon source kitchen and migration pathways that are considerations in hydrocarbon portfolio development, there are several additional technical criteria relevant to CO₂ site portfolios. These criteria include acceptable depth range, proximity to other subsurface management projects such as hydrocarbon production, potable water aquifers, civil infrastructure, the CO₂ sources, as well as potential reservoir size, effectiveness and uncertainty. Various criteria and screening methodologies are available in guideline documents (ISO, 2017; NETL, 2017; Frailey et al., 2018) but these ultimately have to be tailored to local geopolitical and commercial requirements.

Large-scale CO₂ sequestration projects carry significant pressure management requirements due to the volumes in question, especially in the option of CO₂ solution injection (Bryant, 2013; Pool et al., 2013). These can be ameliorated to some degree by choosing to inject into depleted hydrocarbon fields (Jenkins et al., 2012), areas of natural underpressure such as actively deglaciating regions (Bekele and Rostron, 2003), or unconfined aquifers (Sigfusson et al., 2015). The storage volume potential of a prospective CO₂ sequestration site is difficult to estimate due to the absence of storage efficiency information in large-scale projects, and various estimating methodologies are available (De Silva and Ranjith, 2012).

5 Discussion

One important aspect of carbon management to mitigate climate change is geologic carbon storage. Five methods of GCS have been validated through several demonstration and pilot projects around the world: (1) storage in depleted oil and gas fields, (2) use of CO₂ in enhanced hydrocarbon recovery, (3) storage in saline formations/aquifers, (4) injection into deep unmineable coal seams, and (5) *in-situ/ex-situ* carbon mineralization. The role of geoscience in carbon storage

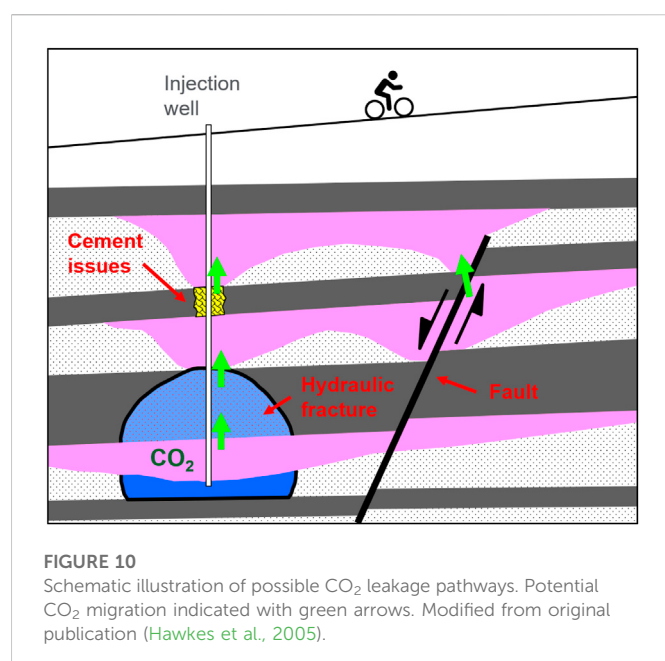


FIGURE 10

Schematic illustration of possible CO₂ leakage pathways. Potential CO₂ migration indicated with green arrows. Modified from original publication (Hawkes et al., 2005).

lies in bringing forward and characterizing prospective CO₂ storage sites. Once a site has been identified, basic subsurface work inevitably entails: (1) reservoir characterization to estimate pore volume and flow behavior, (2) describing the structural geometry to flag potential leak zones, spill points, and fluid pathways along which CO₂ may escape from the intended storage formation, and (3) seal characterization and reservoir pressure to ensure hydraulic integrity.

Selection of any of these five methods requires storage site screening and feasibility studies to ensure project viability. Elaborating on these efforts is beyond the scope of this article. It is useful, however, to distinguish between CO₂ storage options from a site selection and project management perspective as well as considering trapping mechanisms, which are subject to naturally occurring fundamental chemical and geomechanical processes. Once a storage site has been selected for one of the five options we summarized, multiple trapping mechanisms may occur simultaneously or sequentially over time (Figure 8). For example, carbon storage in a saline aquifer or a depleted hydrocarbon field typically begins by injecting CO₂ as a supercritical fluid into a suitable subsurface containment. Initially, structural and stratigraphic trapping of CO₂ as a single-phase fluid occurs as the dominant trapping mechanism. Over time, residual and solubility trapping start contributing as well, and after hundreds to thousands of years, mineral trapping may set in, permanently locking CO₂ in the subsurface by producing new carbon minerals. Not surprisingly, some trapping mechanisms can occur during multiple storage methods as exemplified by *in-situ* carbon mineralization/mineral trapping. However, practical and operational factors during project execution would obviously favor *in-situ* mineralization in suitably mafic rocks and environments where reaction rates are fast (on the order of years) rather than relying on mineral trapping as a minor contributor in mainly subsurface CO₂ fluid storage with considerable uncertainties regarding the timing and amounts of *in-situ* carbon mineralization.

Another way to think about temporal transitions amongst different carbon storage methods is to conduct a simple thought experiment and track a single CO₂ molecule which transitions from one storage option to another. For example, a CO₂ molecule may start off in an enhanced oil or gas recovery operation. At the end of the field life, the CO₂ molecule is trapped in a depleted oil

field. At some point, it will dissolve in the formation brine and ultimately, depending on the availability of Fe and Mg cations, even react to form carbonate minerals. This thought experiment demonstrates that the five storage options summarized above are not necessarily fully separate and that transitions amongst them are likely to occur.

Author contributions

MA—Lead author contributing to all sections SS—Section on characteristic of storage sites, editing RG—Site analysis section and aquifers.

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MA and RG were employed by the company of Aramco Americas, Houston Research Center. SS was employed by the company of Saudi Aramco.

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